

Global sensitivity analysis of backside coating parameters on dynamic response of AM-AFM

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1. Introduction

The Atomic force microscope (AFM) [1] is widely used in engineering science and has found many applications in different sciences. AFM use a micro cantilever as a probe for scanning the sample surface which is externally oscillated close to its resonance frequency in the dynamic modes [2]. The excitations are mostly with harmonically base excitation [3]. Amplitude, phase and resonance frequency are modified by tip-sample interaction forces [2,3]. These changes in oscillation with respect to the external reference oscillation provide information about the sample's characteristics [4]. Dynamic AFM methods are generally divided to Amplitude Modulated Atomic Force Microscope (AM-AFM) [3] and Frequency Modulated Atomic Force Microscope (FM-AFM) [5]. In AM-AFM, ratio of value of amplitude in scanning with free amplitude is the source of contrast. The base excitation amplitude is as large as 20nm to 100nm [2]. This large amount of excitation amplitude cause working the AM-AFM in both the attractive and repulsive regime and so this method names sometimes the Tapping mode [6]. The detection system that has become the standard method for AM-AFM used a laser that is reflected from the backside of the cantilever onto detector. The signal forms the four quadrants of the detector are compared to calculate the deflection signal [7]. Reflectivity or reflectance of cantilever is very important in the quality of received signals by photodiode. In the normal incident the refractive index of silicon nitride with wavelength of 0.3136 μm is 2.148 and the reflectivity of silicon nitride can be calculated 13%. This means just 13% of the incident power is reflected [7]. To improve signal from the cantilevers, they are often sputter coated with a film of various metals in the backside of cantilever [7, 8]. Even a thin coating of a metal can dramatically change the dynamic behaviour of AFM cantilever [9, 10]. By adding a layer of metal coating, the natural resonant frequency of the cantilever will vary [11]. Various coatings are used depending of applications [8, 9, 12, 13]. Different methods of calibration have been proposed where the effect of backside coating is omitted [3, 14-16], however some attempts were done by assuming the coating as an inelastic body for calibration of AFM cantilever [7].

A hybrid method for calibration of AFM cantilevers was introduced where the effects of backside coating is included. The method was based on the minimization of the difference between the Finite Element Method (FEM) and experimentally determined full-field displacement maps of the surface of the cantilever in motion at several resonant frequencies in far away from the sample [17]. When the AFM is far away of the sample the effects of interaction force is negligible and it will not affect dynamic response of system. A systematic investigation of AFM cantilevers coated with several thicknesses of the Diamond like carbon films is studied experimentally in faraway condition. It was demonstrated that for coated cantilevers, the resonance frequency will be determined not only by the properties of the cantilever, but also by the elastic modulus and thickness of the coating [9]. Cantilevers of AFM that uniformly coated with metal thin films between 18 and 73 nm were studied experimentally. An approximate equation for calculating coated AFM cantilever based on Euler Bernoulli theory is introduced while the AFM is faraway of the sample. It was remarked the effect of coating is significant in natural frequency of cantilever [10].

Global sensitivity analysis (GSA) aims at investigating the influence of variations in input parameters on the variation of a model outputs. It can identify contributions of different inputs to the in full distribution domain of the inputs and comprehensively consider the average effect of the inputs on the outputs. GSA can also provide the importance sequence of the model inputs. One type of GSA is the variance-based Sobol' method [18]. In Variance-based method the sensitivity of the output to an input variable is measured by the amount of variance in the output that is caused by that input. Such methods decompose the output variance into parts attributable to individual input variables as well as their interactions. This method has been applied on various models.

For AFM cantilevers, different parameters are studied recently for nano-manipulation [19, 20] piezoelectric micro-cantilever [21], Carbon Nanotube Characteristics in tapping mode [22] and for liquid environments [23]. But in all studies, the interactions between parameters are omitted and just the first order indices discussed.

In current study effects of backside coating parameters including, elastic modulus, thickness, specific mass and Poisson ratio are investigated in AM-AFM. For this approach, Timoshenko beam theory with concentrated tip mass for coated cantilever is derived and the mode shapes of AM-AFM in faraway situation are calculated. The effect of interaction force is modelled by nonlinear general model [24] and assume mode method [25] is used for determination of time response of equations of motion. GSA based on Sobol's statistical method [18, 26] are applied to identify and prioritize the most influential inputs and identify non-influential coating parameters and their interactions on dynamic response of AM-AFM in faraway and scanning situation.

2. Mathematical model

The schematic configuration of AM-AFM is figured in Fig. 1. The extended Hamilton's principle is expressed.

$$\int_{t_1}^{t_2} (\delta T - \delta U + \delta W^{nc}) dt = 0, \quad (1)$$

where T , U and W^{nc} are kinetic energy, strain energy and work by tip-sample interaction force of the system respectively.

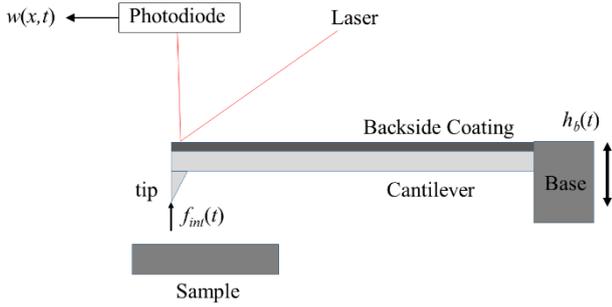


Fig. 1 Schematic of AM-AFM cantilever with backside coating

$$\begin{aligned} T &= \frac{1}{2} \int_0^L \rho_i A_i [\dot{h}_b(t) + \dot{w}(x,t)]^2 dx + \\ &+ \frac{1}{2} m_{tip} [\dot{h}_b(t) + \dot{w}(L,t)]^2 + \frac{1}{2} \int_0^L \rho_i I_i [\dot{\theta}(x,t)]^2 dx; \quad (2) \\ U &= \frac{1}{2} \int_0^L E_i I_i [\theta'(x,t)]^2 dx + \\ &+ \frac{1}{2} \int_0^L k_i A_i G_i [w'(x,t) - \theta(x,t)]^2 dx, \quad (3) \end{aligned}$$

where i is a dummy index and $i = 1$ and 2 are related to substrate/cantilever and coating respectively in the mathematical expression. $w(x,t)$ is relative deflection of cantilever with respect to base and $\theta(x,t)$ is the slope of cantilever that is defined in Timoshenko beam theory. "Prime" and "dot" present the partial derivative with respect to spatial coordinate and time respectively. m_{tip} is the tip mass of cantilever, $f_{in}(t)$ is nonlinear nano-scale tip-sample interaction force and $h_b(t)$ is the base excitation.

The base excitation is assumed a harmonic motion with amplitude equals to Y_0 and frequency equal to resonance frequency of AM-AFM in faraway situation. Other

parameters are introduced in Table 1. The variation of work and energy terms are determined. Integrating over time using integration by parts theorem results the required terms of Eq. (1) as following:

$$\begin{aligned} \int_{t_1}^{t_2} \delta T dt &= - \int_{t_1}^{t_2} \int_0^L \rho_i I_i \ddot{\theta}(x,t) \delta \theta(x,t) dx dt - \\ &- \int_{t_1}^{t_2} m_{tip} [\ddot{h}_b(t) + \ddot{w}(L,t)] \delta w(L,t) dt - \\ &- \int_{t_1}^{t_2} \int_0^L \rho_i A_i [\ddot{h}_b(t) + \ddot{w}(x,t)] \delta w(x,t) dx dt; \quad (4) \end{aligned}$$

$$\begin{aligned} \int_{t_1}^{t_2} \delta U dt &= - \int_{t_1}^{t_2} E_i I_i \theta'(x,t) \delta \theta(x,t) \Big|_0^L dt + \\ &+ \int_{t_1}^{t_2} \int_0^L E_i I_i \theta''(x,t) \delta \theta(x,t) dx dt - \\ &- \int_{t_1}^{t_2} k_i A_i G_i \left\{ [w'(x,t) - \theta(x,t)] \delta w(x,t) \Big|_0^L \right\} dt + \\ &+ \int_{t_1}^{t_2} \int_0^L k_i A_i G_i [w''(x,t) - \theta'(x,t)] \delta w(x,t) dx dt + \\ &+ \int_{t_1}^{t_2} \int_0^L k_i A_i G_i [w'(x,t) - \theta(x,t)] \delta \theta(x,t) dt dx; \quad (5) \end{aligned}$$

$$\begin{aligned} \delta W^{nc} &= f_{in}(t) \delta w(L,t) - \\ &- C \int_0^L \dot{w}'(x,t) \delta w(L,t) dx. \quad (6) \end{aligned}$$

Introducing Eqs. (4)-(5) in to Eq. (1) and using the calculus of variation the two coupled partial equations of motion for Timoshenko beam theory with concentrated end mass [27] for backside coated cantilever are determined:

$$\begin{aligned} \rho_i A_i [\ddot{h}_b(t) + \ddot{w}(x,t)] + C \dot{w}'(x,t) - \\ - k_i A_i G_i [w''(x,t) - \theta'(x,t)] = 0; \quad (7) \end{aligned}$$

$$\begin{aligned} - \rho_i I_i \ddot{\theta}(x,t) + E_i I_i \theta''(x,t) + \\ + k_i A_i G_i [w'(x,t) - \theta(x,t)] = 0. \quad (8) \end{aligned}$$

For the case of clamped-free beam the final form of boundary conditions using Eqs. (4)-(6) are presented as:

$$\theta(0,t) = 0, \quad \theta'(L,t) = 0, \quad w(0,t) = 0; \quad (9)$$

$$\begin{aligned} - m_{tip} [\ddot{h}_b(t) + \ddot{w}(L,t)] - \\ - k_i A_i G_i [w'(L,t) - \theta(L,t)] + f_{in}(t) = 0. \quad (10) \end{aligned}$$

Eq. (10) shows that, the boundary conditions of motion are non-homogeneous, therefore a new variable $Z(x,t)$ is introduced for homogenizing [3, 5].

$$w(x,t) = Z(x,t) + f_{in}(t) g(x). \quad (11)$$

where the function $g(x)$ is chose such the multiplier of $f_{in}(t)$ and $\ddot{f}_{in}(t)$ be eliminated in Eq. (10). Then the function $g(x)$ should satisfy Eqs. (12).

$$g(0) = 0, \quad g(L) = 0, \quad g'(L) = \frac{1}{k_i A_i G_i}. \quad (12)$$

The simplest guess for $g(x)$ is a quadratic function as following which satisfies Eqs. (12).

$$g(x) = \frac{-1}{k_i A_i G_i} x + \frac{1}{k_i A_i G_i L} x^2. \tag{13}$$

Eq. (11) is introduced to higher order PDE which is resulted from the combination of Eqs. (7) and (8). After some calculation the equation of motion is presented as following:

$$\begin{aligned} & -\frac{(\rho_i A_i)(E_i I_i)}{(k_i A_i G_i)(\rho_i I_i)} \ddot{w}''(x, t) + \frac{E_i I_i}{\rho_i I_i} w''''(x, t) + \\ & + \frac{\rho_i A_i}{\rho_i I_i} [\ddot{h}_b(t) + \ddot{w}(x, t)] + \frac{C}{\rho_i I_i} \dot{w}'(x, t) - \\ & - \frac{C.(E_i I_i)}{(k_i A_i G_i)(\rho_i I_i)} \dot{w}'''(x, t) - \dot{w}''(x, t) + \\ & + \frac{\rho_i A_i}{k_i A_i G_i} [\ddot{h}_b(t) + \ddot{w}(x, t)] + \frac{C}{k_i A_i G_i} \ddot{w}'(x, t) = 0. \end{aligned} \tag{14}$$

Assumed mode method [25] is used on $Z(x, t)$. Here $\varphi_i(x)$ are mode functions of AM-AFM in faraway condition and $q_i(t)$ are generalized coordinates.

$$Z(x, t) = \sum_{k=1}^N \varphi_k(x) q_k(t). \tag{15}$$

The mode shapes of monolayer undamped Timoshenko beam with concentrated end mass has been solved analytically [28]. The same process are applied to coated cantilever. After some mathematical calculation, the characteristic equation is determined as:

$$\begin{aligned} & \left(\frac{\alpha^2 + s^2}{\alpha}\right) (R_3 R_4' - R_3' R_4 + R_4 R_1' - R_1 R_4') + \\ & + \left(\frac{\beta^2 - s^2}{\beta}\right) (R_2 R_3' - R_2' R_3 + R_1 R_2' - R_2 R_1') = 0, \end{aligned} \tag{16}$$

where

$$\left[\begin{matrix} \alpha \\ \beta \end{matrix} \right] = \frac{\sqrt{2}}{2} \left\{ \mp (r^2 + s^2) + \left[(r^2 - s^2)^2 + \frac{4}{b^2} \right]^{1/2} \right\}^{1/2}; \tag{17}$$

$$\left. \begin{aligned} R_1 &= (b/\alpha) \sinh(b\alpha) + M_n b^2 \cosh(b\alpha); \\ R_2 &= (b/\alpha) \cosh(b\alpha) + M_n b^2 \sinh(b\alpha); \\ R_3 &= (b/\beta) \sin(b\beta) + M_n b^2 \cos(b\beta); \\ R_4 &= -(b/\beta) \cos(b\beta) + M_n b^2 \sin(b\beta); \end{aligned} \right\} \tag{18}$$

$$\left. \begin{aligned} R_1' &= \left(\frac{\alpha^2 + s^2}{\alpha}\right) b\alpha \cosh(b\alpha); \\ R_2' &= \left(\frac{\alpha^2 + s^2}{\alpha}\right) b\alpha \sinh(b\alpha); \\ R_3' &= -\left(\frac{\beta^2 - s^2}{\beta}\right) b\beta \cos(b\beta); \\ R_4' &= -\left(\frac{\beta^2 - s^2}{\beta}\right) b\beta \sin(b\beta). \end{aligned} \right\} \tag{19}$$

The non-dimensional variables are defined as:

$$\left. \begin{aligned} \xi &= \frac{x}{L}; \quad b = \frac{\rho_i A_i}{E_i I_i} L^4 \omega^2; \quad r^2 = \frac{\rho_i I_i}{\rho_i A_i L^2}; \\ s^2 &= \frac{E_i I_i}{k_i A_i G_i L^2}; \quad M_n = \frac{M}{\rho_i A_i L}. \end{aligned} \right\} \tag{20}$$

The mode shapes of coated AM-AFM in faraway situation is determined as:

$$\begin{aligned} \varphi(\xi) &= \Phi \left[\cosh(b\alpha\xi) - \frac{(R_1 - R_3)}{(R_2 - RR_4)} \sinh(b\alpha\xi) - \right. \\ & \left. - \cos(b\beta\xi) + \frac{R(R_1 - R_3)}{(R_2 - RR_4)} \sin(b\beta\xi) \right], \end{aligned} \tag{21}$$

where Φ is a constant and:

$$R = \frac{(\alpha^2 + s^2)}{\alpha} \frac{\beta}{(\beta^2 - s^2)}. \tag{22}$$

Introducing Eq. (11) and (15) to Eq. (14) using the orthogonality of mode functions and integrating over length of cantilever the final form of ODEs are determined as following after some mathematical calculations:

$$\begin{aligned} & G_j \ddot{q}_k'' + D_{kj} \ddot{q}_k'' + (C_{kj} + I_j) \ddot{q}_k'' + \\ & (B_{kj} + E_{kj}) \dot{q}_k' + A_{kj} q_k + F_j \ddot{h}_b + \\ & H_j \ddot{h}_b + O_j \ddot{f}_{int}(t) + M_j \ddot{f}_{int}(t) + \\ & + (L_j + P_j) \dot{f}_{int}(t) + (K_j + N_j) \dot{f}_{int}(t) + \\ & + J_j f_{int}(t) = 0, \end{aligned} \tag{23}$$

where j is free indices and k is dummy indices which means summation over k and other parameters are noted in Eqs. (24)-(25).

$$\left. \begin{aligned} A_{kj} &= \frac{E_i I_i}{\rho_i I_i} \int_0^L \varphi_k'''' \varphi_j dx; \\ B_{kj} &= -\frac{C(E_i I_i)}{(k_i A_i G_i)(\rho_i I_i)} \int_0^L \varphi_k'''' \varphi_j dx; \\ C_{kj} &= -\left[\frac{(\rho_i A_i)(E_i I_i)}{(k_i A_i G_i)(\rho_i I_i)} + 1 \right] \times \int_0^L \varphi_k'' \varphi_j dx; \\ D_{kj} &= \frac{C}{k_i A_i G_i} \int_0^L \varphi_k' \varphi_j dx; \\ E_{kj} &= \frac{C}{\rho_i I_i} \int_0^L \varphi_k' \varphi_j dx; \\ F_j &= \frac{\rho_i A_i}{k_i A_i G_i} \int_0^L \varphi_k dx; \\ G_j &= \frac{\rho_i A_i}{k_i A_i G_i} \int_0^L \varphi_j^2 dx; \end{aligned} \right\} \tag{24}$$

$$\left. \begin{aligned}
 H_j &= \frac{\rho_i A_i}{\rho_i I_i} \int_0^L \varphi_j dx; \\
 I_j &= \frac{\rho_i A_i}{\rho_i I_i} \int_0^L \varphi_j^2 dx; \\
 J_j &= \frac{E_i I_i}{\rho_i I_i} \int_0^L g'''(x) \varphi_j dx; \\
 K_j &= -\frac{C(E_i I_i)}{(k_i A_i G_i)(\rho_i I_i)} \int_0^L g'''(x) \varphi_j dx; \\
 L_j &= -\left[\frac{(\rho_i A_i)(E_i I_i)}{(k_i A_i G_i)(\rho_i I_i)} + 1 \right] \times \\
 &\quad \times \int_0^L g''(x) \varphi_j dx; \\
 M_j &= \frac{C}{k_i A_i G_i} \int_0^L g'(x) \varphi_j dx; \\
 N_j &= \frac{C}{\rho_i I_i} \int_0^L g'(x) \varphi_j dx; \\
 O_j &= \frac{\rho_i A_i}{k_i A_i G_i} \int_0^L g(x) \varphi_j dx; \\
 P_j &= \frac{\rho_i A_i}{\rho_i I_i} \int_0^L g(x) \varphi_j dx.
 \end{aligned} \right\} \quad (25)$$

The nonlinear nanoscale tip-sample interaction force is modeled via general force [24]:

$$f_{in}(t) = a_a [D(t)]^{\gamma_a} + a_r [D(t)]^{\gamma_r}, \quad (26)$$

where a_a , a_r , γ_a and γ_r denote the attractive and repulsive amplitude and power terms, respectively. $D(t)$ is tip-sample distance and is related to $w(x, t)$ as:

$$D(t) = w_{set} + h_b(t) + w(L, t), \quad (27)$$

where w_{set} is set/approach point of AM-AFM probe. Eq. (27) is reduced to Eq. (28) at $x = L$.

$$D(t) = w_{set} + h_b(t) + Z(L, t). \quad (28)$$

The cross sectional area of AM-AFM cantilever is usually assumed as rectangular shape [3, 7, 14] however in practice most AFM cantilevers deviate from the rectangular cross section and they mostly have a trapezoidal cross section [8, 17] which is due to dynamic etching effect on rectangular cantilevers.

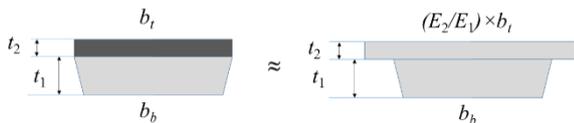


Fig. 2 Transformed cross section of trapezoidal cross section of AM-AFM cantilever

In current research trapezoidal cross section is assumed with b_b and b_t for bottom wide and top wide of trapezoidal cross section respectively which are showed in Fig. 2. It should be remarked that in all equations I is calculated for transform cross section of bilayer cantilever that is showed in Fig. 2. The details of calculation of transformed

cross section can be find in text books and are not noted here.

3. GSA by Sobol Method

The mathematical model of AM-AFM is nonlinear and when the model is nonlinear and non-monotonic, the decomposition of the output variance is still defined and can be used [29]. The model input vector is denoted in Eq. (29) for Y as output of system. It is assumed $Y = f(\Psi)$ is a square integrable function. It is possible to represent this function as a sum of elementary functions [18].

$$\begin{aligned}
 Y = f(\Psi) &= f_0 + \sum_{i=1}^d f_i(\Psi_i) + \sum_{i<j}^d f_{ij}(\Psi_i, \Psi_j) + \\
 &\quad + \dots + f_{123\dots d}(\Psi); \quad (29)
 \end{aligned}$$

$$\Psi = (\Psi_1, \Psi_2, \dots, \Psi_d) \in R^d. \quad (30)$$

This expansion is unique under conditions:

$$\begin{aligned}
 \int_0^1 f_{i_1 i_2 \dots i_s}(\Psi_{i_1}, \Psi_{i_2}, \dots, \Psi_{i_s}) d\Psi_{i_k} &= 0, \\
 1 \leq k \leq s, \{i_1, \dots, i_s\} &\subseteq \{1, 2, \dots, d\}. \quad (31)
 \end{aligned}$$

This implies that f_0 is a constant. It is showed a functional decomposition of the variance is available for output that often is referred to as functional ANalysis Of VAriances (ANOVA).

$$Var(Y) = f_0 + \sum_{i=1}^d D_i(Y) + \sum_{i<j}^d D_{ij}(Y) + \dots + D_{123\dots d}(Y); \quad (32)$$

$$D_i(Y) = Var[\mathbb{E}(Y|\Psi_i)]; \quad (33)$$

$$D_{ij}(Y) = Var[\mathbb{E}(Y|\Psi_i, \Psi_j)] - D_i(Y) - D_j(Y), \quad (34)$$

where \mathbb{E} denotes expected value that is defined in mathematical symbols.

For higher order interactions, the similar mathematical process in Eqs. (33) and (34) is needed. The so-called Sobol indices or variance based sensitivity indices [18] are obtained. These indices express the share of variance of Y that is due to a given input or inputs combination.

$$S_i = \frac{D_i(Y)}{Var(Y)}, S_{ij} = \frac{D_{ij}(Y)}{Var(Y)}, \dots \quad (35)$$

There are $2^d - 1$ indices. The total indices or total effects are introduced as follows:

$$S_{(i)}^{tot} = S_i + \sum_{j \neq i} S_{ij} + \sum_{i \neq j, j \neq k, j < k} S_{ijk} + \dots = \sum_{l \in \#i} S_l, \quad (36)$$

where $\#i$ are all the subsets of $\{1, 2, \dots, d\}$ including i . In practice, when d is large, only the main effects and the total effects are computed, thus giving a good information on the model sensitivities. The most informative situations are noted in Eqs. (37)-(38). Eq. (37) means the output is independent of i th variable and Eq. (38) shows that the output is

dependent of i th variable only. The difference between these two values stated on interaction of one input parameters with other input parameters.

$$S_{(i)}^{tot} = S_i = 0 ; \quad (37)$$

$$S_{(i)}^{tot} = S_i = 1 . \quad (38)$$

4. Numerical results and discussions

Numerical results for presented model is investigated for a case study. The specifications of AM-AFM cantilever are tabulated in Table 1 that are adopted from [17]. In each problem the excitation frequency of base is set as the resonance frequency of same problem. w_{set} is set 60 nm and Y_0 is assumed 60 nm. This large amount of base amplitude assures that the cantilever works in attractive and repulsive force regimes both [2]. Magnitude of nonlinear nanoscale tip sample interaction force is adopted from [24] for scanning condition.

Verification of model is checked with comparing with experimental and theoretical results in [17] that are tabulated in Table 2. The results of present model is tabulated in Table 3 for three different assumptions. Percent of error is defined as average of absolute deviation of each mode with respected to experimental data in the same mode.

Table 1

List of parameters of AM-AFM cantilever

Parameter	Value	Description	Unit
L	474	Length	μm
b_t	53	Top Wide	μm
b_b	50	Bottom Wide	μm
t_1	1.66	Cantilever Tickness	μm
t_2	30	Coating Tickness	nm
E_1	160	Cantilever Elastic Mod.	Gpa
E_2	68	Coating Elastic Mod.	Gpa
ν_1	0.27	Cantilever Poisson Ratio	-
ν_2	0.38	Coating Poisson Ratio	-
k_1	0.8484	Cantilever Shear Factor	-
k_2	0.8529	Coating Shear Factor	-
ρ_1	2329	Cantilever Specific Mass	Kg/m^3
ρ_2	2698.9	Coating Specific Mass	Kg/m^3
m_{tip}	0	Tip mass	Kg
a_a	-1×10^{-29}	Attractive Amplitude term	-
a_r	1×10^{-86}	Repulsive Amplitude Term	-
γ_a	-2	Attractive Power Term	-
γ_r	-8	Repulsive Power Term	-

It is seen that the present model can predict the experimental data in good accuracy and effect of backside coating is important even in the range of 30 nm. As it is seen in Table 3 if the tip length assumed shorter but the effect of tip mass entered the error is decreased to lower range. To investigate the effects of backside coating different physical range of related parameters are studied. The minimum and maximum of parameters are tabulated in Table 4.

Table 2

Resonance frequency in KHz adopted from [17]

Mode	Experiment	FEM	Theory
#1	9.978	9.978	9.939
#2	62.620	62.265	62.286
#3	174.800	174.567	174.401
#4	343.000	342.354	341.110
#5	567.500	566.909	564.949
#6	848.000	848.053	843.936
Error(%)	0.000	0.304	0.677

Table 3

Resonance frequency in KHz for present model

Mode	Present Model		
	$L = 474 \mu\text{m}$ Uncoated	$L = 474 \mu\text{m}$ Coated	$L = 470 \mu\text{m}$ Coated+ $M_n = 1\%$
#1	9.886	9.996	9.973
#2	61.948	62.639	62.535
#3	173.442	175.375	175.177
#4	339.831	343.617	343.408
#5	561.667	567.920	567.859
#6	838.854	848.186	848.500
Error(%)	0.859	0.246	0.171

Table 4

Physical rang of backside coating parameters

Parameter	Minimum	Maximum	Unit
t_2	0	500	nm
E_2	0	700	Gpa
ρ_2	0	25000	Kg/m^3
ν_2	0	0.5	-

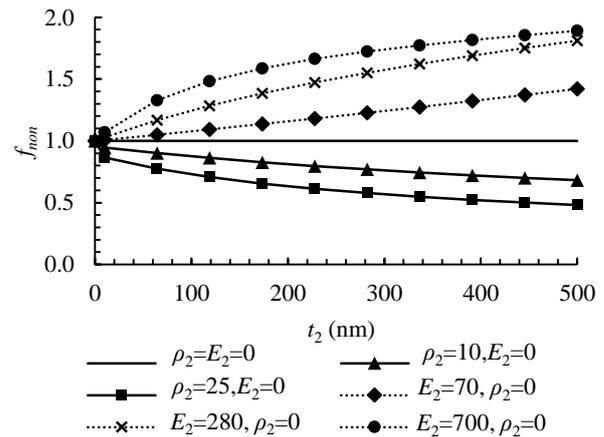


Fig. 3 Variation of f_{non} with t_2 for inelastic and massless assumption of coating (E_2 is in Gpa and ρ_2 in g/cm^3)

f_{non} is defined as the resonance frequency of each problem divided to resonance frequency of first mode of uncoated AM-AFM cantilever (here 9.8856 KHz). Two important assumption are the inelastic ($E_2 = 0$) assumption and massless ($\rho_2 = 0$) assumption for coating. These two assumptions are plotted in Fig. 1 for f_{non} . Fig. 3 demonstrates that these assumption are not valid for proper modelling of

coating effects even for small thickness. The inelastic assumption is under estimated and the massless assumption is over estimated in prediction of f_{non} .

GSA based on Sobol method is applied to f_{non} as output of dynamic system when the cantilever is faraway of the sample by coding in MATLAB. The Sobol indices and total indices of backside coating parameters are plot in Fig. 4. Results demonstrate that the effect of coating's Poisson Ratio is negligible in output and the most important factor is ρ_2 , however the effect of E_2 is important too. Thus in next steps the effect of Poisson ratio is neglected.

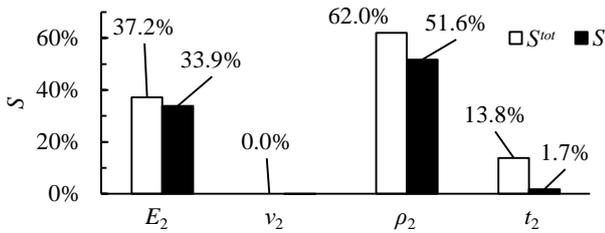


Fig. 4 Sensitivity indices for backside coating parameters for f_{non} as output

To calculate the amplitude of response, time domain response of cantilever is determined by coding in MATLAB and amplitude of response in excitation frequency is calculated by Fast Fourier Transform (FFT) of time response. Sampling frequency of FFT is set such that the frequency resolution remains minimum in 10 Hz level. This process is applied to both scanning and faraway conditions of AM-AFM. The magnitude of amplitude in faraway condition and in scanning condition is defined A_0 and A_1 respectively for each problem. The ratio of A_1/A_0 is defined A_{non} that is the monitoring signal in AM-AFM [2, 3].

Fig. 5 shows variation of A_{non} while the thickness of backside coating is assumed 100nm. Different coating that are frequently used for AM-AFM are showed as a surface in this situation. It should be remarked that the value of A_{non} is lower than unit for uncoated AM-AFM cantilever. This reduction is due to effect of nonlinear tip-sample interaction force. It is seen value of A_{non} is decreased with coating effects. The amount of this reduction is significant when comparing it with the decrease of amplitude for uncoated cantilever. A_{non} is waned generally with the increase of elastic modulus and specific mass.

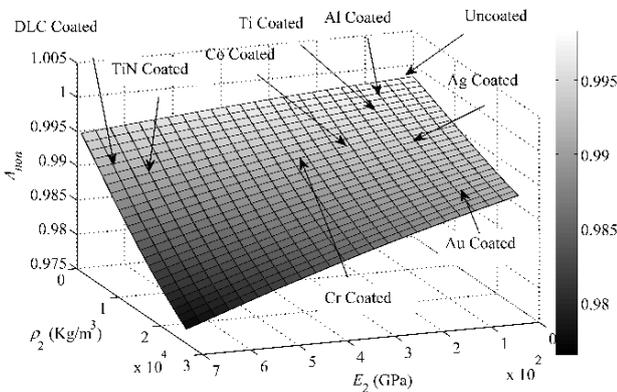


Fig. 5 Variation of A_{non} in fixed magnitude of $t_2 = 100$ nm

In Fig. 6 E_2 is assumed as the elastic modulus of chrome (E_{Cr}) and the effects of t_2 and ρ_2 on A_{non} is figured.

It is seen with increasing the magnitude of both t_2 and ρ_2 the nonlinearity of monitoring signal is increased, however in low amount of t_2 (about 10 nm) the changes in A_{non} is inclined to linear. The trend is always decreasing.

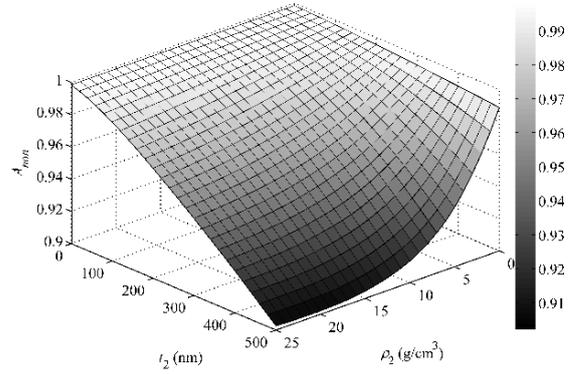


Fig. 6 Variation of A_{non} in fixed magnitude of $E_2 = E_{Cr}$

In Fig. 7 ρ_2 is assumed constant equal to the specific mass of Gold ($\rho_2 = \rho_{Au}$). Quantitatively changes in A_{non} for different values of E_2 seems linear. Again, changes in A_{non} are more linear in small value of t_2 . Generally, the non-linear trend is seen in Figs. 3-5.

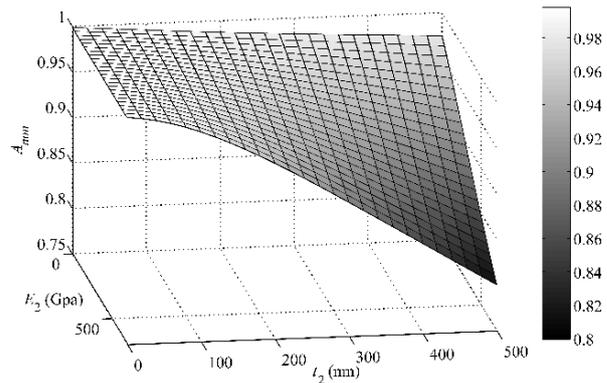


Fig. 7 Variation of A_{non} in fixed magnitude of $\rho_2 = \rho_{Au}$

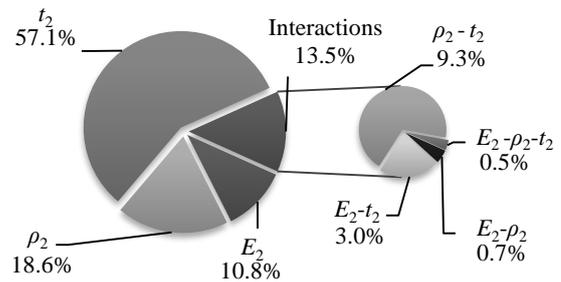


Fig. 8 Sobol indices of backside coating parameters for A_0 as output of dynamic system

Here the Sobol indices and total indices are determined for A_{non} and A_0 . This process is applied for these two different outputs for an important reason. Authors observed in their results that the effect of backside coating is different for A_0 and A_1 . This different amplitude of response for faraway condition and scanning situation demonstrate that backside coating parameters affects the output signal of AM-AFM.

Fig. 8 shows the Sobol indices for A_0 as output. In this case t_2 and ρ_2 and E_2 are the most influencing parameters

for the model output variance according to first order index. The sum of first order indices of the parameters shows 86.5% which illustrate high interaction between studied parameters. Between the all interaction indices the share of thickness and density interaction is the most important and the third order interaction is negligible.

Fig. 9 shows the same indices for the monitoring signal of AM-AFM. The value of indices are different in all cases for A_{non} but the sequence of most influence parameters are remained the same as for A_0 . The changes in indices of E_2 and ρ_2 are neglectable. The variations are important in indices related to t_2 and interaction terms. The change is decreasing for t_2 . Between all interaction indices the most change is related to thickness and specific mass interaction that is increasing. These changes demonstrate that the non-linear nano-scale tip sample force affects the amount of A_{non} due to backside coating and the dynamic response is different for scanning and faraway situations.

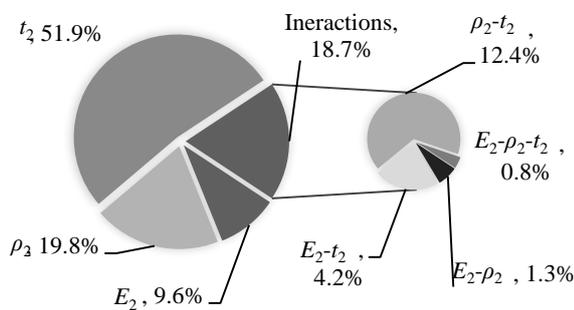


Fig. 9 Sobol indices of backside coating parameters for A_{non} as output of dynamic system

The comparison of first order Sobol indices and total indices are plotted for both outputs in Fig. 10. The total sensitivity index in Fig. 10 shows that the S^{tot} has a consistent trend as the S , that is, the ranking of parameters by first order values agreed well with those from S^{tot} values. It is seen that all the S^{tot} values are greater than first order indices. This again suggests each parameter interacts as a pair, or more with the other parameters that is discussed previously. The value of S^{tot} for both inputs have negligible changes for t_2 . This is because of decreasing the first order and increasing of interactions related to t_2 that is caused for little change in total index. The most change for total index is seen for ρ_2 .

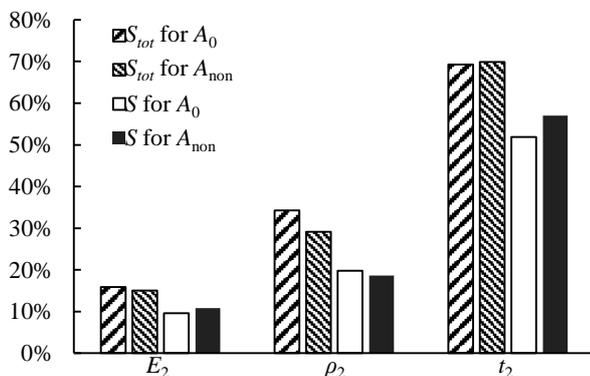


Fig. 10 Comparison of sensitivity indices for backside coating parameters for A_0 and A_{non} as output

5. Conclusions

In this study, mathematical model of AM-AFM cantilever was derived based on Timoshenko beam theory with concentrated end mass. Effect of backside coating was included using extended Hamiltonian principle. The general form of nano-scale nonlinear tip-sample interaction force was involved as time variant boundary condition problem. The equations of motion were homogenized and combined to high order coupled PDEs of motion. The trapezoidal cross section was assumed for AM-AFM cantilever and all the calculations were applied for transformed cross section of area. Mode shapes of problem were derived for coated cantilever. The GSA based on Sobol's method was introduced which is able to predict the interaction of input parameters for dynamic nonlinear systems. In the faraway situation the natural frequency of coated cantilever was calculated for a case study and was validated with experimental results in literature. It was showed the error is lower for shorter cantilever with tip mass. The results were compared with previously introduced theoretical models too. Physical range of backside coating parameters were introduced. Two well-known assumptions (inelastic and massless assumptions) were plotted. It was demonstrated that, these assumptions are not proper choice for modelling of coating effects in AM-AFM and the effect of backside coating should not neglect in mathematical modeling of AM-AFM. GSA on these parameters were applied to non-dimensional resonance frequency for faraway situation. It was showed the effect of Poisson ratio of coating is negligible. For a constant value of every coating parameters the variation of non-dimension amplitude in scanning condition was investigated. It is showed qualitatively that for small magnitude of coating thickness the behavior is inclined linear. First order and total indices of backside coating parameters for faraway and scanning situation of AM-AFM were determined and compared. It was showed the sequence of indices remains unchanged for both cases and the most important parameters are thickness, specific mass and elastic modulus of coating respectively. However, the value of indices are different for each condition. It was showed the interactions between parameters are important in variance of outputs and the related indices are large enough. Comparison between the first order indices and total indices were discussed. It was remarked difference between the GSA indices for faraway and scanning situation shows that the effect of coating is different in both condition.

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GLOBAL SENSITIVITY ANALYSIS OF BACKSIDE
COATING PARAMETERS ON DYNAMIC RESPONSE
OF AM-AFM

S u m m a r y

Influence of backside coating parameters on dynamic response of AM-AFM is modeled. Timoshenko based beam model is used and the general nonlinear interaction force is enclosed. The coupled ODEs of motion are

achieved. The mode shapes are determined for coated cantilever and the natural frequency of each mode is validated with experimental results. It is showed a shorter cantilever with tip mass have better accuracy and inelastic and massless assumptions are not proper choice for modelling of the coating. The assumed mode method is used to determine time response of system for faraway and scanning condition of AM-AFM. Amplitude of response is calculated by FFT of time domain. Sensitivity indices of backside coating parameters are determined based on Sobol method in their physical range. It is showed the sequence of indices remains unchanged. The most important parameters and interactions on output variance are introduced. The results are concluded.

Keywords: AM-AFM, Global sensitivity analysis, Nonlinear vibration, Coated cantilever, Backside Coating parameters, Timoshenko beam theory

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